Microwave Imaging from Total Electric Field Data

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Abstract—A novel gradient-based inverse scattering method for imaging inhomogeneous objects from time-domain data of only total electric field is presented. Unlike most inverse scattering methods, the proposed method does not require the explicit information of the incident field illuminating a region of interest. Numerical simulations demonstrate the effectiveness of the method.

I. INTRODUCTION

Most inverse scattering methods assume the knowledge of incident fields illuminating an region of interest [1]-[3]. We have proposed an inverse scattering approach which does not require the information of the incident field [4]. The approach uses both total electric and magnetic fields data. We have also reported reconstruction from only total electric field data using an generic algorithm (GA) as an optimization method [5]. Due to the computational complexity, GAs are not suitable for the reconstruction of complex and/or inhomogeneous objects.

In this paper, we consider the imaging of inhomogeneous objects. A gradient-based optimization is applied to the inverse scattering analysis using only total electric field data. Numerical simulations are carried out to show the effectiveness of the method.

II. DIRECT PROBLEM

Let us consider the scattering problem where an region of interest is illuminated by the incident field produced by an impressed electric current $J$ which is turned on at the time $t=0$.

A. Original Scattering Problem

The total electromagnetic fields $v=[E, \eta H]$ are the solution of the following problem:

$$L \cdot v(r,t) = j(r,t), \quad r \in \mathbb{R}^3, \quad t \in (0, \infty)$$

initial condition: $v(r,0) = 0, \quad r \in \mathbb{R}^3$

where $j=[\eta J, 0]$, and $\eta = \sqrt{\mu_0/\varepsilon_0}$ is the characteristic impedance of free space. The operator $L$ is defined by

$$L = \tilde{A} \frac{\partial}{\partial x} + \tilde{B} \frac{\partial}{\partial y} + \tilde{C} \frac{\partial}{\partial z} - \tilde{F} \frac{\partial}{\partial (ct)} - \tilde{G}$$

(2)

where $c(=1/\sqrt{\varepsilon_0 \mu_0})$ is the speed of light in free space, $\tilde{A}, \tilde{B}, \tilde{C}$ are $6 \times 6$ constant matrices and $\tilde{F}, \tilde{G}$ are $6 \times 6$ matrices contain electrical parameters (the relative permittivity $\varepsilon_r$, relative permeability $\mu_r$, and conductivity $\sigma$) of the medium. For more details, please refer to [6].

B. Equivalent Problem

The original problem is equivalent to the following interior boundary value problem whose solution $v_{eq}=[E^{eq}, \eta H^{eq}]$ is identical to $v$ of the original problem (1) in the interior region $\Omega$ bounded by the observation surface $\partial \Omega$ where the total electric field $E$ of the original problem is measured:

$$L \cdot v_{eq}(r,t) = 0, \quad r \in \Omega, \quad t \in (0, \infty)$$

initial condition: $v_{eq}(r,0) = 0, \quad r \in \Omega$

boundary condition:

$$\hat{n} \times (E^{eq}(r,t) \times \hat{n}) = \hat{n} \times (E(r, t) \times \hat{n}), \quad r \in \partial \Omega, \quad t \in (0, \infty).$$

C. Time Reversal Problem

By time-reversing the measured data of total electric field $E$ on the observation surface $\partial \Omega$, a time reversal problem where the time-reversed field $v^r=[E^r, \eta H^r]$ is equivalent to $v$ of the original problem in the interior region $\Omega$ is set up provided that the measurement duration time $T$ is long enough for the fields in the interior region $\Omega$ to be negligibly small after the time $T$. The time-revered field $v^r$ is the solution of the following boundary value problem:

$$L \cdot v^r(r,t) = 0, \quad r \in \Omega, \quad t \in (0, T)$$

final condition: $v^r(r,T) = 0, \quad r \in \Omega$

boundary condition:

$$\hat{n} \times (E^r(r,t) \times \hat{n}) = \hat{n} \times (E(r, t) \times \hat{n}), \quad r \in \partial \Omega, \quad t \in (0, T).$$

III. INVERSE SCATTERING PROBLEM

Let us consider the imaging problem of the electrical parameter profiles of objects of interest from the recorded data of the total electric field on the observation surface $\partial \Omega$. Note that the equivalent field and the time-reversed field is the same as the original total field generated by the impressed current $J$ placed exterior to the surface $\partial \Omega$ if and only if the medium in $\Omega$ is the same as the original one. Using this fact, we reduce the inverse scattering problem considered here to the optimization problem minimizing the following cost functional:
The reconstructed region is a 3

cylinder of inner radius

and outer radius

is an electrical parameter

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and the time factor

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with the time factor

The reconstructed result after 500 iterations is shown in

Fig. 1(b). This shows that the proposed method gives an

accurate reconstruction.

The second example is the reconstruction of two different rectangular cylinders as shown in Fig. 2(a). The relative permittivity, size, and center location of each cylinder are

\( \varepsilon_{r1} = 2.0, 0.7\lambda \times 1.2\lambda, (x = -0.5\lambda, y = 0.5\lambda) \) and

\( \varepsilon_{r2} = 2.0, 0.7\lambda \times 0.7\lambda, (x = 0.5\lambda, y = -0.5\lambda) \), respectively. The reconstructed result after 500 iterations is shown in Fig. 2(b).

Again, it can be seen that the proposed method is very effective.

\( \frac{d}{dt} = \frac{\alpha}{(\tau + \beta)^3} \exp \left[ -\alpha^2 (t - \tau)^2 \right] \)  \hspace{1cm} (7)

where \( \tau = (\beta + 400)\Delta t \), \( \alpha = 5.6/(\beta \Delta t) \) and \( \beta = 132 \) with the time step size \( \Delta t = 0.98(\Delta x/c \sqrt{2}) = 10.4 \text{ ps} \) and the cell size \( \Delta x = \Delta y = \lambda/10\sqrt{4} = 4.5 \text{ mm} \). Here, \( \lambda = 90 \text{ mm} \) is the wavelength in free space at the highest frequency where the source spectrum is 1/20 of the maximum value. The computational domain is discretized into 180×180 cells. Twelve sources are placed on the boundary line of the 5λ×5λ square and are successively used to probe the cylinder. The tangential components of the total electric fields are collected on the periphery of the 4λ×4λ square surrounding the object. The reconstructed region is a 3λ×3λ square.

The first example is the reconstruction of a hollow circular cylinder of inner radius \( a = 0.3\lambda \) and outer radius \( b = \lambda \) (see Fig. 1(a)). Its relative permittivity has a sine-like profile with maximum value 2:

\[ \varepsilon_r(r) = \begin{cases} \sin \left( \frac{\pi (r-a)}{b-a} \right) + 1 & a \leq r \leq b \\ 1 & \text{otherwise.} \end{cases} \]  \hspace{1cm} (8)

The reconstructed result after 500 iterations is shown in

Fig. 1(a). It’s relative permittivity has a sine-like profile with maximum value 2:

\[ \varepsilon_r(r) = \begin{cases} \sin \left( \frac{\pi (r-a)}{b-a} \right) + 1 & \text{otherwise.} \end{cases} \]  \hspace{1cm} (8)

REFERENCES


IV. NUMERICAL RESULTS

In order to assess the proposed method, numerical simulations of reconstructing two-dimensional lossless dielectric objects are carried out. In the simulations presented here, the primary source is a z-directed line current source \( J = I(t)\hat{z} \) with the time factor

\[ I(t) = \frac{d^3}{dt^3} \exp \left[ -\alpha^2 (t - \tau)^2 \right] \]  \hspace{1cm} (7)

where \( \tau = (\beta + 400)\Delta t \), \( \alpha = 5.6/(\beta \Delta t) \) and \( \beta = 132 \) with the time step size \( \Delta t = 0.98(\Delta x/c \sqrt{2}) = 10.4 \text{ ps} \) and the cell size \( \Delta x = \Delta y = \lambda/10\sqrt{4} = 4.5 \text{ mm} \). Here, \( \lambda = 90 \text{ mm} \) is the wavelength in free space at the highest frequency where the source spectrum is 1/20 of the maximum value. The computational domain is discretized into 180×180 cells. Twelve sources are placed on the boundary line of the 5λ×5λ square and are successively used to probe the cylinder. The tangential components of the total electric fields are collected on the periphery of the 4λ×4λ square surrounding the object. The reconstructed region is a 3λ×3λ square.

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Fig. 1(b). This shows that the proposed method gives an accurate reconstruction.